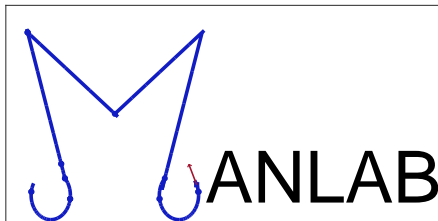


# The Asymptotic Numerical Method in *Manlab-4*

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- 2 Elements of theory on the ANM
- 3 Concrete examples
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# Aim of the talk :

Describe the so-called **Asymptotic Numerical Method**,  
a **continuation method**  
using high order **Taylor series** expansions.



# Continuation

Goal : determine solution branches of

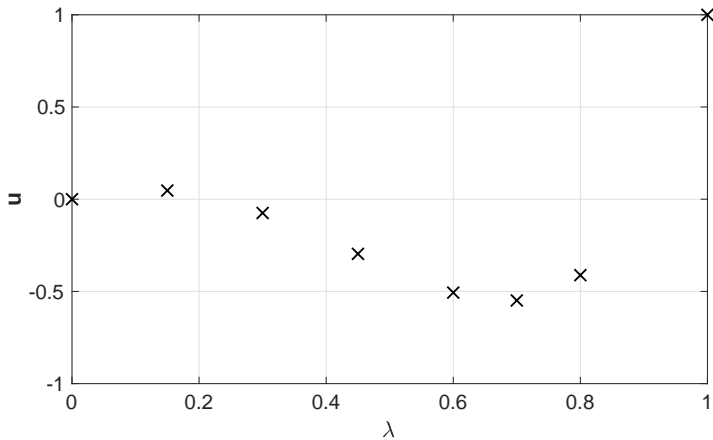
$$\mathbf{R}(\mathbf{u}, \lambda) = 0$$

with  $\mathbf{u} \in \mathbb{R}^n$  and  $\lambda \in \mathbb{R}$

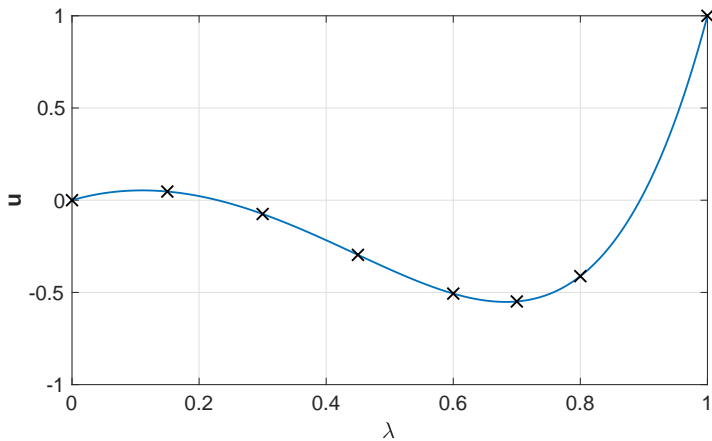
and  $\mathbf{R} : \mathbb{R}^{n+1} \mapsto \mathbb{R}^n$  is a smooth function.



# Continuation



# Continuation



# The cornerstone

To compute the **Taylor series** of the solution-branch :

- Insert the **Taylor series**

$$u(a) = u_0 + a u_1 + a^2 u_2 + \cdots + a^N u_N$$

- Into the **algebraic equation**

$$R(u, \lambda) := u + u^2 + \frac{\tan(u)}{1 + u} - \lambda = 0$$

- And collect terms with the same powers !



# Live demonstration.



# Logistic Map

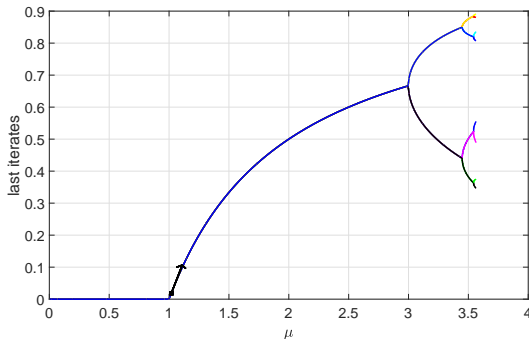
Compute the iterates of the logistic map

$$f(x) = \mu x(1 - x)$$

The system solved is

$$\left\{ \begin{array}{l} x_1 = f(x_0) \\ x_2 = f(x_1) \\ \vdots \\ x_{N-1} = f(x_{N-2}) \\ x_N = f(x_{N-1}) \end{array} \right.$$

with  $x_0 = 0.5$  and  $N = 5000$ .



# Pendulum

Compute the orbit of the pendulum

$$\begin{cases} \dot{\theta} &= \phi \\ \dot{\phi} &= -\sin(\theta) \end{cases}$$

with  $\theta(0) = \frac{\pi}{2}$  and  $\phi(0) = 0$ . The system is solved with a  $\lambda$ -scheme :

$$\begin{cases} \theta_{n+1} &= \theta_n + h\phi_{n+\lambda} \\ \phi_{n+1} &= \phi_n - h\sin(\theta_{n+\lambda}) \end{cases}$$

with  $x_{n+\lambda} = (1-\lambda)x_n + \lambda x_{n+1}$ , and  $h = \frac{2\pi}{100}$ .



# Pendulum

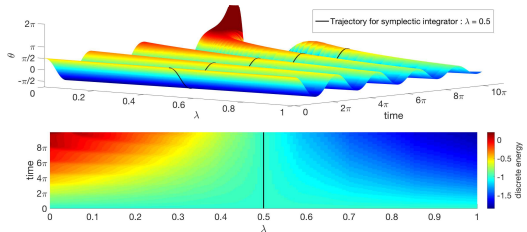
Compute the orbit of the pendulum

$$\begin{cases} \dot{\theta} &= \phi \\ \dot{\phi} &= -\sin(\theta) \end{cases}$$

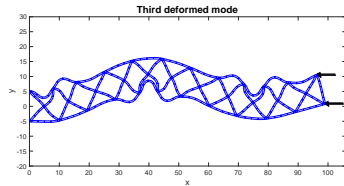
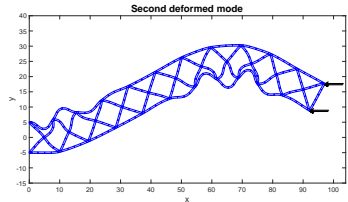
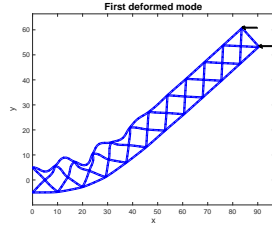
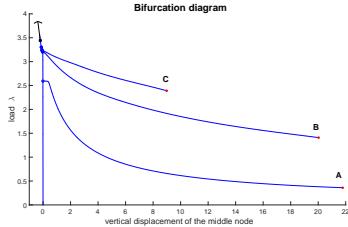
with  $\theta(0) = \frac{\pi}{2}$  and  $\phi(0) = 0$ . The system is solved with a  $\lambda$ -scheme :

$$\begin{cases} \theta_{n+1} &= \theta_n + h\phi_{n+\lambda} \\ \phi_{n+1} &= \phi_n - h\sin(\theta_{n+\lambda}) \end{cases}$$

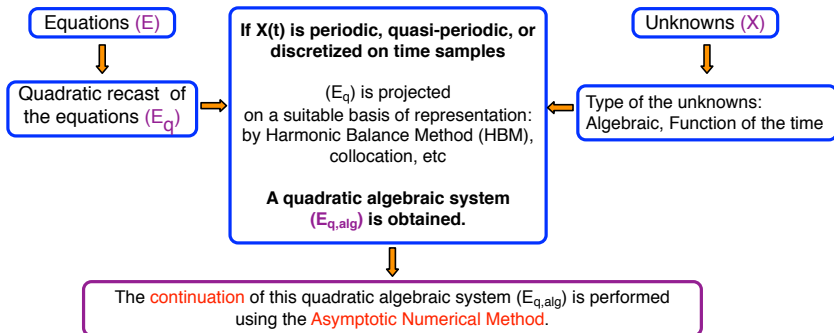
with  $x_{n+\lambda} = (1-\lambda)x_n + \lambda x_{n+1}$ , and  $h = \frac{2\pi}{100}$ .



# Deformation of a complex structure



# Overview of *Manlab-4*



# Continuation

Goal : determine solution branches of

$$\mathbf{R}(\mathbf{U}) = \mathbf{R}(\mathbf{u}, \lambda) = 0$$

where  $\mathbf{U} = [\mathbf{u}, \lambda]$ .

with  $\mathbf{u} \in \mathbb{R}^n$  and  $\lambda \in \mathbb{R}$

and  $\mathbf{R} : \mathbb{R}^{n+1} \mapsto \mathbb{R}^n$  is a smooth function.



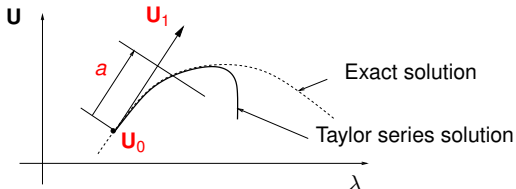
# Taylor series based continuation

- let  $\mathbf{U}_0$  be a regular point with  $\|\mathbf{R}(\mathbf{U}_0)\| < \varepsilon_R$  (tolerance).
- let  $\mathbf{U}_1$  be the tangent at  $\mathbf{U}_0$ .
- let  $a$  be the pseudo arc length parameter  $a = \mathbf{U}_1^T \cdot (\mathbf{U} - \mathbf{U}_0)$ .

**Implicit Function theorem** : The solution branch passing through  $\mathbf{U}_0$  may be represented as a (truncated) Taylor series with respect to the pseudo-arclength parameter  $a$ .

$$\mathbf{U}(a) = \mathbf{U}_0 + a\mathbf{U}_1 + a^2\mathbf{U}_2 + \cdots + a^N\mathbf{U}_N \quad \text{and } N = 20 \text{ or } 30$$

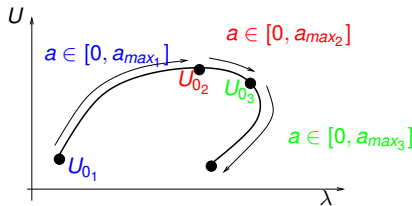
**Series computation** : solve a succession of linear systems that share the same stiffness matrix  $\frac{\partial \mathbf{R}}{\partial \mathbf{U}} \mathbf{U}_p = F_p^{nl}(\mathbf{U}_1, \dots, \mathbf{U}_{p-1})$



The **Domain of utility** of the series is the interval  $[0, a_{max}]$  for which  $\|\mathbf{R}(\mathbf{U}(a))\| < \varepsilon_R$

A good approximation :  $\mathbf{R}(\mathbf{U}_0 + \dots + a^N \mathbf{U}_N) \simeq \mathbf{R}(\mathbf{U}_0) + a^{N+1} \mathbf{R}^{N+1}$ ,

So, if one requires  $\|a^{N+1} \mathbf{R}^{N+1}\| < \varepsilon_R$  then  $a_{max} = \left( \frac{\varepsilon_R}{\|\mathbf{R}^{N+1}\|} \right)^{\frac{1}{N+1}}$



The complete solution branch is obtained as a succession of local Taylor series

$$\mathbf{U}(a) = \mathbf{U}_0 + a\mathbf{U}_1 + a^2\mathbf{U}_2 + \dots + a^N\mathbf{U}_N \quad \text{avec} \quad a \in [0, a_{max}]$$

- piece-wise continuous representation
- **auto-adaptative** step length → Robustness
- no algorithmic parameter



# The cornerstone

To compute the Taylor series of the solution-branch :

- Insert the Taylor series

$$u(a) = u_0 + a u_1 + a^2 u_2 + \cdots + a^N u_N$$

- Into the algebraic equation

$$R(u, \lambda) := u + u^2 + \frac{\tan(u)}{1 + u} - \lambda = 0$$

- And collect terms with the same powers !

**Two techniques :**

- use **Automatic Differentiation** to do the job : nice for the user but poor efficiency.
- do a **quadratic recast** of the equations : then the job becomes easy and efficient



# Quadratic recast

How to recast the algebraic system  $\mathbf{R}(\mathbf{U}) = 0$  in a quadratic way ?

- Goal : find auxiliary variables  $\mathbf{U}_a$  and  $\mathbf{R}_f$  such that

$$\mathbf{R}_f(\mathbf{U}_f) = \mathbf{C} + \mathbf{L}(\mathbf{U}_f) + \mathbf{Q}(\mathbf{U}_f, \mathbf{U}_f)$$

- with  $\mathbf{U}_f = (\mathbf{U}, \mathbf{U}_a)$ ,
- $\mathbf{C}$  constant,
- $\mathbf{L}$  linear,
- $\mathbf{Q}$  quadratic.

Note that  $\mathbf{R}_f(\mathbf{U}_f) = \begin{bmatrix} \mathbf{R}(\mathbf{U}_f) \\ \mathbf{R}_a(\mathbf{U}_f) \end{bmatrix}$  with  $\frac{\partial \mathbf{R}_a}{\partial \mathbf{U}_a}$  invertible and  $\mathbf{R}(\mathbf{U}_f) = \mathbf{R}(\mathbf{U})$ .



# The examples of the pendulum

Dimensionless parameters :  $m = 1$  and  $g = 1$ .

Energy of the system :

$$H(\theta) = 1 - \cos(\theta) + \frac{k}{2}(\theta - \frac{\pi}{M})^2$$

Equation of the motion :

$$\ddot{\theta} + \sin(\theta) + k(\theta - \frac{\pi}{M}) = 0$$

Steps :

- $M = 2$  is constant, development about  $\theta = 0$  :

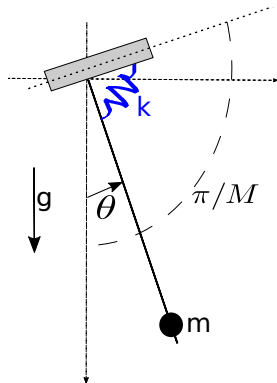
$$\ddot{\theta} + \theta - \frac{\theta^3}{6} + k(\theta - \frac{\pi}{2}) = 0$$

- $k = 0.1$  is constant, development about  $\theta = 0$  :

$$\ddot{\theta} + \theta - \frac{\theta^3}{6} + 0.1(\theta - \frac{\pi}{M}) = 0$$

- Without simplification :

$$\ddot{\theta} + \sin(\theta) + k(\theta - \frac{\pi}{M}) = 0$$



# How to recast polynomials quadratically ?

Let  $\mathbf{R}(\mathbf{U}) = \mathbf{R}(u, \lambda) = u^3 + u + 1 - \lambda$ .

Let  $v = u^2$ .

$\mathbf{U} = (u, \lambda)$  and  $\mathbf{U}_a = v$  then  $\mathbf{U}_f = (\mathbf{U}, \mathbf{U}_a) = (u, \lambda, v)$ .

Then  $\mathbf{R}_f$  is defined :

$$\mathbf{R}_f(\mathbf{U}_f) = \mathbf{R}_f(u, \lambda, v) = \begin{bmatrix} uv + u + 1 - \lambda \\ v - u^2 \end{bmatrix}$$

And the operators are  $\mathbf{C} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$ ,  $\mathbf{L}(\mathbf{U}_f) = \begin{bmatrix} u - \lambda \\ v \end{bmatrix}$ ,  $\mathbf{Q}(\mathbf{U}_f, \mathbf{U}_f) = \begin{bmatrix} uv \\ -u^2 \end{bmatrix}$ .



# Basic example : Simplified Pendulum

Pendulum subject to an angular spring at position  $\theta = \frac{\pi}{2}$ , developed around  $\theta = 0$ .  
The equilibrium is given by :

$$r(\theta, k) = \left(\theta - \frac{\theta^3}{6}\right) + k\left(\theta - \frac{\pi}{2}\right)$$

Definition of the auxiliary variables

$$\psi = \theta^2$$

Yields the quadratic recast

$$\mathbf{R}_f(\mathbf{U}_f) = \mathbf{R}_f(\theta, k, \psi) = \begin{bmatrix} \theta - \frac{\theta\psi}{6} + k\theta - k\frac{\pi}{2} \\ \psi - \theta^2 \end{bmatrix}$$

And the operators are  $\mathbf{C} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$ ,  $\mathbf{L}(\mathbf{U}_f) = \begin{bmatrix} \theta - k\frac{\pi}{2} \\ \psi \end{bmatrix}$ ,  $\mathbf{Q}(\mathbf{U}_f, \mathbf{U}_f) = \begin{bmatrix} -\frac{\theta\psi}{6} \\ -\theta^2 \end{bmatrix}$ .



# How to recast fractions quadratically?

Let  $\mathbf{R}(\mathbf{U}) = \mathbf{R}(u, \lambda) = \frac{1}{u} + u - \lambda$ .

Let  $v = \frac{1}{u}$ .  $v$  can be defined implicitly through  $uv = 1$ .

Then  $\mathbf{R}_f$  is defined :

$$\mathbf{R}_f(\mathbf{U}_f) = \mathbf{R}_f(u, \lambda, v) = \begin{bmatrix} v + u - \lambda \\ uv - 1 \end{bmatrix}$$

And the operators are  $\mathbf{C} = \begin{bmatrix} 0 \\ -1 \end{bmatrix}$ ,  $\mathbf{L}(\mathbf{U}_f) = \begin{bmatrix} u + v - \lambda \\ 0 \end{bmatrix}$ ,  $\mathbf{Q}(\mathbf{U}_f, \mathbf{U}_f) = \begin{bmatrix} 0 \\ uv \end{bmatrix}$ .

Here,  $\mathbf{R}_a(\mathbf{U}_f) = uv - 1$  and  $\frac{\partial \mathbf{R}_a}{\partial \mathbf{U}_a} = \frac{\partial \mathbf{R}_a}{\partial v} = u$ . It is invertible if and only if  $u \neq 0$ .



# Simple example : Another Simplified Pendulum

Pendulum subject to an angular spring at position  $\theta = \frac{\pi}{M}$ , developed around  $\theta = 0$ .  
The equilibrium is given by :

$$r(\theta, M) = \left(\theta - \frac{\theta^3}{6}\right) + 0.1\left(\theta - \frac{\pi}{M}\right)$$

Definition of the auxiliary variables

$$\begin{aligned}\psi &= \theta^2 \\ M_{inv} &= \frac{1}{M}\end{aligned}$$

Yields the quadratic recast

$$\mathbf{R}_f(\mathbf{U}_f) = \mathbf{R}_f(\theta, M, \psi, M_{inv}) = \begin{bmatrix} \theta - \frac{\theta\psi}{6} + 0.1(\theta - M_{inv}\pi) \\ \psi - \theta^2 \\ M_{inv}M - 1 \end{bmatrix}$$



# How to recast **everything else** quadratically ?

Let  $\mathbf{R}(\mathbf{U}) = \mathbf{R}(u, \lambda) = u - \tan(u) - \lambda$ . Let  $t = \tan(u)$  and let  $z = 1 + t^2$ .  $t$  and  $z$  can be defined by the system :

$$\begin{aligned} dt &= z du \\ z &= 1 + t^2 \end{aligned}$$

These equations are quadratic with respect to the Taylor coefficients of  $u, t$  and  $z$ . Then  $\mathbf{R}_f$  and its differential form  $d\mathbf{R}_f$  are defined :

$$\mathbf{R}_f(\mathbf{U}_f) = \mathbf{R}_f(u, \lambda, t, z) = \begin{bmatrix} u - t - \lambda \\ t - \tan(u) \\ z - 1 - t^2 \end{bmatrix} \quad d\mathbf{R}_f(\mathbf{U}_f, d\mathbf{U}_f) = \begin{bmatrix} \text{Not needed} \\ dt - z du \\ \text{Not needed} \end{bmatrix}$$

And the operators are  $\mathbf{C} = \begin{bmatrix} 0 \\ 0 \\ -1 \end{bmatrix}$ ,  $\mathbf{L}(\mathbf{U}_f) = \begin{bmatrix} u - t - \lambda \\ 0 \\ z \end{bmatrix}$ ,  $\mathbf{Q}(\mathbf{U}_f, \mathbf{U}_f) = \begin{bmatrix} 0 \\ 0 \\ -t^2 \end{bmatrix}$ ,

$$d\mathbf{L}(d\mathbf{U}_f) = \begin{bmatrix} 0 \\ dt \\ 0 \end{bmatrix} \text{ and } d\mathbf{Q}(\mathbf{U}_f, d\mathbf{U}_f) = \begin{bmatrix} 0 \\ -z du \\ 0 \end{bmatrix}.$$



# Transcendental example : Pendulum

Pendulum subject to an angular spring at position  $\theta = \frac{\pi}{M}$ .  
The equilibrium is given by :

$$r(\theta, k, M) = \sin(\theta) + k(\theta - \frac{\pi}{M})$$

Definition of the auxiliary variables, together with the differentiated forms (when needed) :

$$\begin{aligned} s &= \sin(\theta) & ds &= c d\theta \\ c &= \cos(\theta) & dc &= -s d\theta \\ M_{inv} &= \frac{1}{M} \end{aligned}$$

Define  $\mathbf{U}_f = (\theta, k, M, s, c, M_{inv})$  yields the "quadratic" recast

$$\mathbf{R}_f(\mathbf{U}_f) = \begin{bmatrix} s + k(\theta - M_{inv}\pi) \\ s - \sin(\theta) \\ c - \cos(\theta) \\ M_{inv}M - 1 \end{bmatrix} \quad d\mathbf{R}_f(\mathbf{U}_f, d\mathbf{U}_f) = \begin{bmatrix} \text{Not needed} \\ ds - cd\theta \\ dc + sd\theta \\ \text{Not needed} \end{bmatrix}$$



# End of the Algebraic elements of theory.



# Taylor series algebra

- Product of Taylor series  $u(a) \times v(a)$  :

$$\begin{aligned} & (u_0 + au_1 + a^2u_2 + \cdots + a^Nu_N) \times (v_0 + av_1 + a^2v_2 + \cdots + a^Nv_N) \\ &= u_0v_0 + a(u_1v_0 + u_0v_1) + a^2(u_2v_0 + u_1v_1 + u_0v_2) + \cdots + a^N \sum_{j=0}^N u_{N-j}v_j \end{aligned}$$

It is truncated at order  $N$ .

- Differentiation of Taylor series  $\frac{\partial u}{\partial a}(a)$  :

$$\frac{\partial}{\partial a} (u_0 + au_1 + a^2u_2 + \cdots + a^Nu_N) = u_1 + 2au_2 + 3a^2u_3 + \cdots + Na^{N-1}u_N$$

The constant coefficient  $u_0$  is not anymore in the development, that goes now up to order  $N - 1$ .



# Manlab 4.0

Let  $R(\mathbf{U}) = 0$  be

$$\begin{aligned} r_1(u_1, u_2, \lambda) &= 2u_1 - u_2 + 100 \frac{u_1}{1+u_1+u_1^2} - \lambda = 0 \\ r_2(u_1, u_2, \lambda) &= 2u_2 - u_1 + 100 \frac{u_2}{1+u_2+u_2^2} - (\lambda + \mu) = 0 \end{aligned}$$

Introduce the auxiliary variables :

$$\begin{aligned} v_1 &= 1 + u_1 + u_1 u_1 \\ v_2 &= 1 + u_2 + u_2 u_2 \\ v_3 &= 1/v_1 \\ v_4 &= 1/v_2 \end{aligned}$$

- All these expression are quadratic, or easily made quadratic
- "linear declaration rule" : an auxiliary variable  $v_i$  cannot appear on the left hand side before it has been explicitly defined as  $v_i = f(\mathbf{U}, v_1, v_2, \dots, v_{i-1})$ . Ensures that  $\frac{\partial \mathbf{R}_a}{\partial \mathbf{U}_a}$  is invertible.

Let  $\mathbf{U}_a = [v_1, v_2, v_3, v_4]$  be the vector of auxiliary variables

Let  $\mathbf{U}_f = [\mathbf{U}, \mathbf{U}_a]$



# Manlab 4.0

The original system  $R(\mathbf{U}) = 0$  is replaced by the equivalent quadratic one  $\mathbf{R}(\mathbf{U}_f)$

$$\begin{aligned} r_1 &:= 2u_1 - u_2 + 100u_1v_3 - \lambda &= 0 \\ r_2 &:= 2u_2 - u_1 + 100u_2v_3 - (\lambda + \mu) &= 0 \\ r_{aux1} &:= v_1 - 1 + u_1 + u_1 * u_1 &= 0 \\ r_{aux2} &:= v_2 - 1 + u_2 + u_2 * u_2 &= 0 \\ r_{aux3} &:= v_3 * v_1 - 1 &= 0 \\ r_{aux4} &:= v_4 * v_2 - 1 &= 0 \end{aligned}$$

Tensor formalism : this quadratic system may be written

$$R_i = C_i + L_{ij}U_j + Q_{ijk}U_jU_k \quad i, j, k = 1, 2, \dots, n$$

with  $C, L, Q$  being tensors of order 1, 2 and 3

Here, we have 7 components  $C_i$ , 49 components  $L_{ij}$  and 343 components  $Q_{ijk}$ .

But most of them are zero !



# Manlab 4.0 : Sparse tensor formalism

The sparse tensor  $C$ ,  $L$  and  $Q$  are defined by the following lists (as in Matlab for a sparse matrix)

- order 1 tensor  $C$

```
iC= [ 2 5 6 ]  
vC= [-μ -1 -1 ]
```

- order 2 tensor  $L$

```
iL= [1 1 1 2 2 2 3 3 4 4 5 6 ]  
jL= [1 2 7 1 2 7 1 3 2 4 5 6 ]  
vL= [2 -1 -1 -1 2 -1 -1 1 -1 1 1 1 ]
```

- order 3 tensor  $Q$

```
iQ= [ 1 2 3 4 5 6 ]  
jQ= [ 1 2 1 2 3 4 ]  
kQ= [ 5 6 1 2 5 6 ]  
vQ= [100 100 -1 -1 1 1 ]
```

In Manlab 4.0, these lists are **automatically generated** from the quadratic system.



# Manlab 4.0 : Sparse tensor formalism

How to get the lists defining the sparse tensor, from the quadratic expression  
 $R(X) := 0$ ?

Polarization formula :

$$C = R(0)$$

$$L(X) = \frac{1}{2} (R(X) - R(-X))$$

$$Q(X, Y) = \frac{1}{4} (R(X + Y) - R(X - Y) - R(Y) + R(-Y))$$



## Manlab 4.0 : Sparse tensor formalism

Using these lists, the computation of the residual vector  $R(\mathbf{U}) = C + L(\mathbf{U}) + Q(\mathbf{U}, \mathbf{U})$  stand in one (Matlab) line.

```
R =sparse(iC,ones(1,size(iC,2)),vC',neq,1)  
+ sparse(iL,ones(1,size(iL,2)),vL'.*U(jL),neq,1)  
+ sparse(iQ,ones(1,size(iQ,2)),vQ'.*(U(jQ).*U(kQ)),neq,1)
```

For the jacobian matrix  $dRdU = L(.) + Q(\mathbf{U},.) + Q(.,\mathbf{U})$

```
dRdU = sparse(iL,jL,sys.vL,neq,ninc)  
+ sparse(iQ,kQ,vQ'.*U(jQ),neq,ninc)  
+ sparse(iQ,jQ,vQ'.*U(kQ),neq,ninc)
```



# Manlab 4.0 : Condensation

The linear problem to be solved at each order  $p$  reads :

$$\begin{bmatrix} B & A_{aux} \\ A & C \end{bmatrix} \begin{bmatrix} \mathbf{U} \\ \mathbf{U}_{aux} \end{bmatrix} = \begin{bmatrix} F_{aux\ p} \\ F_p \end{bmatrix} \quad \begin{array}{l} \leftarrow R_{aux} \\ \leftarrow R \end{array}$$

Thanks to the "linear declaration rule", the matrix  $A_{aux}$  is triangular which allows an easy and cheap block solving

We first solve

$$\begin{bmatrix} A - C A_{aux}^{-1} B \end{bmatrix} \begin{bmatrix} U \end{bmatrix} = \begin{bmatrix} F_p - C A_{aux}^{-1} F_{aux\ p} \end{bmatrix}$$

where  $\begin{bmatrix} A - C A_{aux}^{-1} B \end{bmatrix}$  is the jacobian matrix of the original (non quadratic) system.



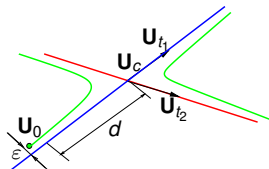
# Bifurcation detection using series analysis

Numerical evidence : near a simple bifurcation, a **geometric series** emerge in the Taylor series.

$$\mathbf{U}(a) = \mathbf{U}_0 + a \mathbf{U}_1 + a^2 \mathbf{U}_2 + a^3 \mathbf{U}_3 + \dots$$

First order analysis : expression of a perturbed branches near a simple bifurcation [Cochelin & Médale, 2013]

$$\mathbf{U}(a) = \mathbf{U}_0 + a \mathbf{U}_{t_1} - \varepsilon \frac{\frac{a}{d}}{(1 - \frac{a}{d})} \mathbf{U}_{t_2}$$



- $\frac{\frac{a}{d}}{1 - \frac{a}{d}} = \frac{a}{d} + (\frac{a}{d})^2 + (\frac{a}{d})^3 + \dots$ , a geometric serie with common ratio  $\frac{1}{d}$
- After each Taylor series computation, we look for an emerging geometric series. When detected , it is extracted, completed to infinity and replaced by a fraction

$$\mathbf{U}(a) = \underbrace{\mathbf{U}_0 + a \hat{\mathbf{U}}_1 + a^2 \hat{\mathbf{U}}_2 + \dots + a^{n-1} \hat{\mathbf{U}}_{n-1}}_{\hat{\mathbf{U}}(a) \text{ cleaned series}} + \frac{a}{d} \left( \frac{1}{1 - \frac{a}{d}} \right) \mathbf{U}_{scale}$$

We get  $d$ ,  $\mathbf{U}_{t_2}$  and can go further the bifurcation thanks to the cleaned series.

