

The Asymptotic Numerical Method in *Manlab-4*

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Aim of the talk :

Describe the so-called **Asymptotic Numerical Method**,
a **continuation method**
using high order **Taylor series** expansions.



Continuation

Goal : determine solution branches of

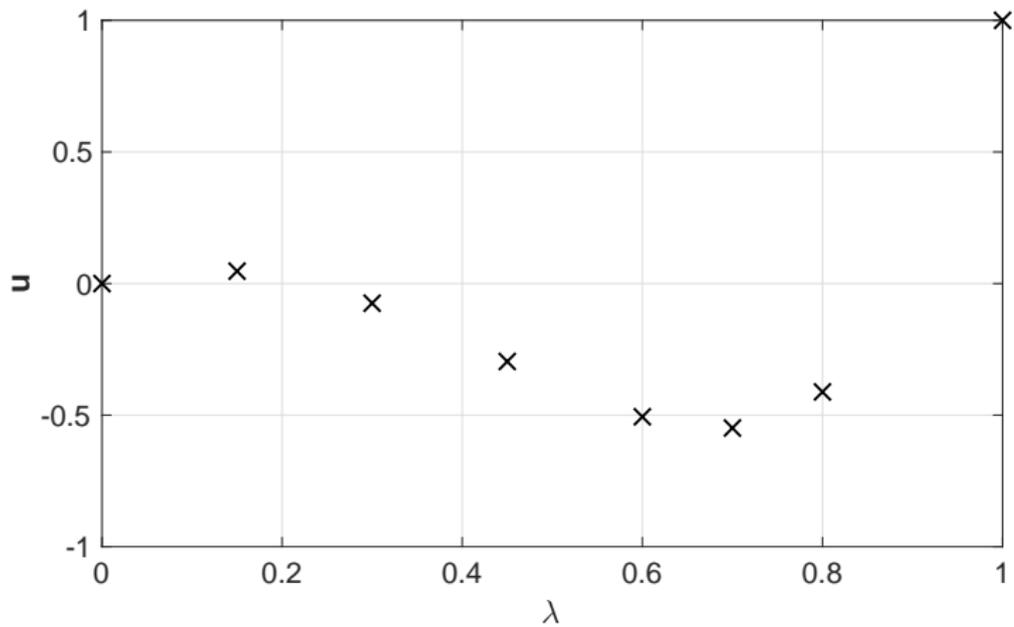
$$\mathbf{R}(\mathbf{u}, \lambda) = 0$$

with $\mathbf{u} \in \mathbb{R}^n$ and $\lambda \in \mathbb{R}$

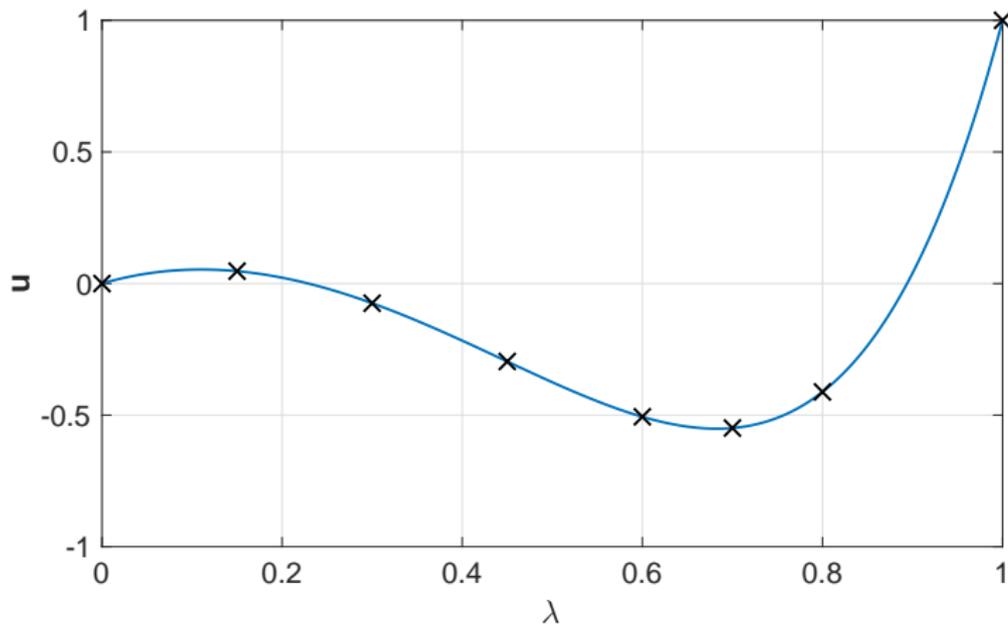
and $\mathbf{R} : \mathbb{R}^{n+1} \mapsto \mathbb{R}^n$ is a smooth function.



Continuation



Continuation



The cornerstone

To compute the **Taylor series** of the solution-branch :

- Insert the **Taylor series**

$$u(a) = u_0 + a u_1 + a^2 u_2 + \cdots + a^N u_N$$

- Into the **algebraic equation**

$$R(u, \lambda) := u + u^2 + \frac{\tan(u)}{1 + u} - \lambda = 0$$

- And collect terms with the same powers !



Live demonstration.



Logistic Map

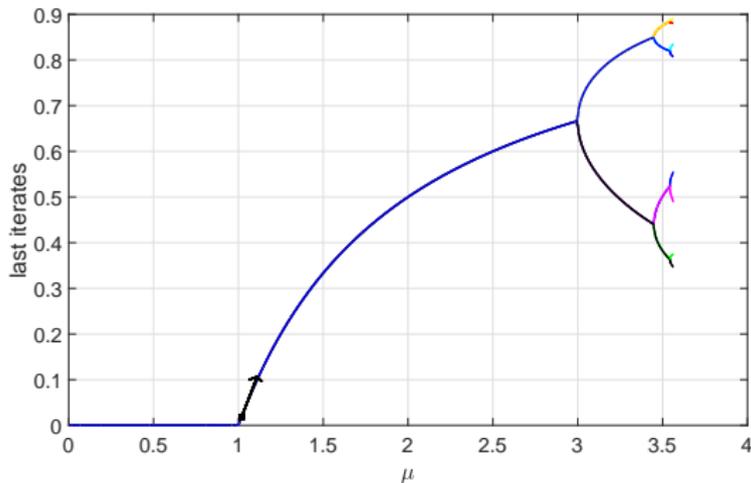
Compute the iterates of the logistic map

$$f(x) = \mu x(1 - x)$$

The system solved is

$$\left\{ \begin{array}{l} x_1 = f(x_0) \\ x_2 = f(x_1) \\ \vdots \\ x_{N-1} = f(x_{N-2}) \\ x_N = f(x_{N-1}) \end{array} \right.$$

with $x_0 = 0.5$ and $N = 5000$.



Pendulum

Compute the orbit of the pendulum

$$\begin{cases} \dot{\theta} &= \phi \\ \dot{\phi} &= -\sin(\theta) \end{cases}$$

with $\theta(0) = \frac{\pi}{2}$ and $\phi(0) = 0$. The system is solved with a λ -scheme :

$$\begin{cases} \theta_{n+1} &= \theta_n + h\phi_{n+\lambda} \\ \phi_{n+1} &= \phi_n - h\sin(\theta_{n+\lambda}) \end{cases}$$

with $x_{n+\lambda} = (1-\lambda)x_n + \lambda x_{n+1}$, and
 $h = \frac{2\pi}{100}$.



Pendulum

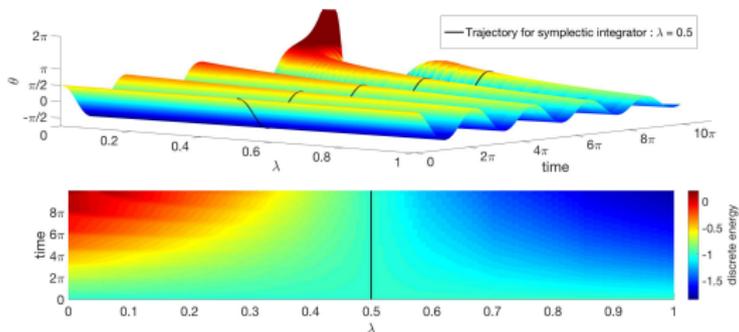
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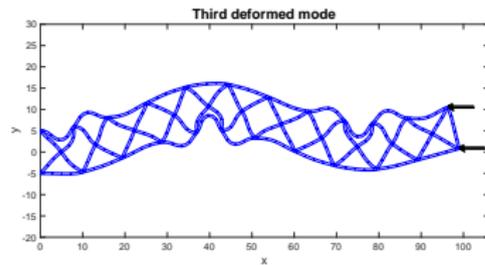
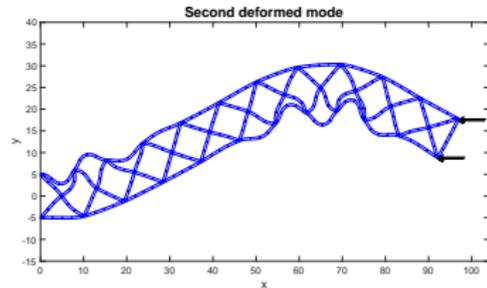
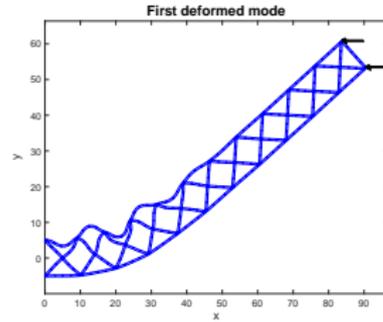
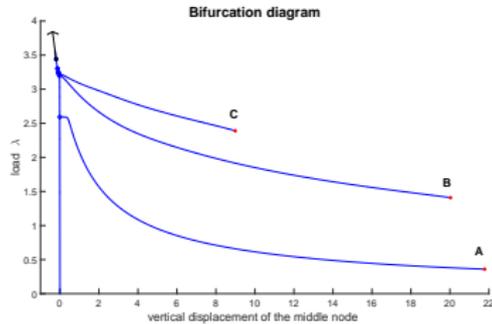
with $\theta(0) = \frac{\pi}{2}$ and $\phi(0) = 0$. The system is solved with a λ -scheme :

$$\begin{cases} \theta_{n+1} &= \theta_n + h\phi_{n+\lambda} \\ \phi_{n+1} &= \phi_n - h\sin(\theta_{n+\lambda}) \end{cases}$$

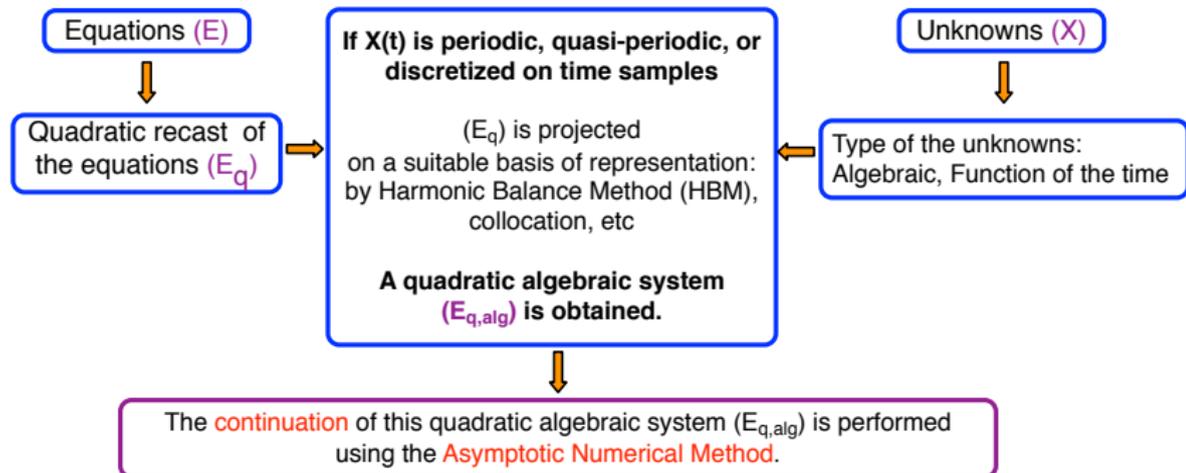
with $x_{n+\lambda} = (1-\lambda)x_n + \lambda x_{n+1}$, and $h = \frac{2\pi}{100}$.



Deformation of a complex structure



Overview of *Manlab-4*



Continuation

Goal : determine solution branches of

$$\mathbf{R}(\mathbf{U}) = \mathbf{R}(\mathbf{u}, \lambda) = 0$$

where $\mathbf{U} = [\mathbf{u}, \lambda]$.

with $\mathbf{u} \in \mathbb{R}^n$ and $\lambda \in \mathbb{R}$

and $\mathbf{R} : \mathbb{R}^{n+1} \mapsto \mathbb{R}^n$ is a smooth function.



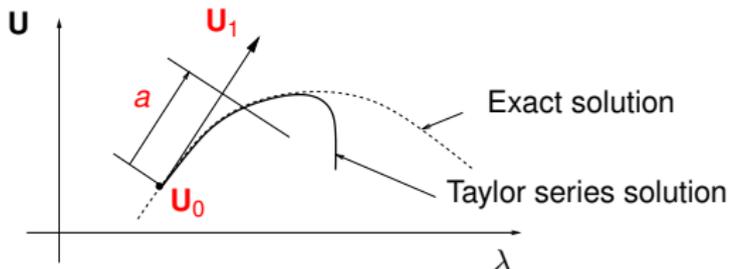
Taylor series based continuation

- let \mathbf{U}_0 be a regular point with $\|\mathbf{R}(\mathbf{U}_0)\| < \varepsilon_R$ (tolerance).
- let \mathbf{U}_1 be the tangent at \mathbf{U}_0 .
- let a be the pseudo arc length parameter $a = \mathbf{U}_1^T \cdot (\mathbf{U} - \mathbf{U}_0)$.

Implicit Function theorem : The solution branch passing through \mathbf{U}_0 may be represented as a (truncated) Taylor series with respect to the pseudo-arclength parameter a .

$$\mathbf{U}(a) = \mathbf{U}_0 + a\mathbf{U}_1 + a^2\mathbf{U}_2 + \dots + a^N\mathbf{U}_N \quad \text{and } N = 20 \text{ or } 30$$

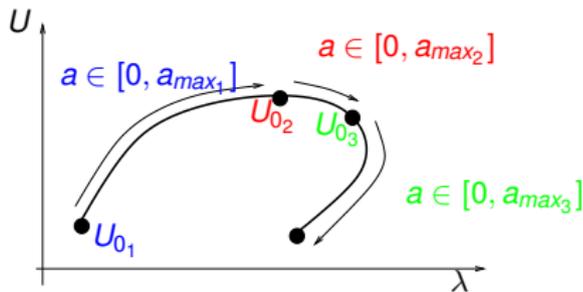
Series computation : solve a succession of linear systems that share the same stiffness matrix $\frac{\partial \mathbf{R}}{\partial \mathbf{U}} \mathbf{U}_p = F_p^{nl}(\mathbf{U}_1, \dots, \mathbf{U}_{p-1})$



The **Domain of utility** of the series is the interval $[0, a_{max}]$ for which $\|\mathbf{R}(\mathbf{U}(a))\| < \varepsilon_R$

A good approximation : $\mathbf{R}(\mathbf{U}_0 + \dots + a^N \mathbf{U}_N) \simeq \mathbf{R}(\mathbf{U}_0) + a^{N+1} \mathbf{R}^{N+1}$,

So, if one requires $\|a^{N+1} \mathbf{R}^{N+1}\| < \varepsilon_R$ then $a_{max} = \left(\frac{\varepsilon_R}{\|\mathbf{R}^{N+1}\|} \right)^{\frac{1}{N+1}}$



The complete solution branch is obtained as a succession of local Taylor series

$$\mathbf{U}(a) = \mathbf{U}_0 + a\mathbf{U}_1 + a^2\mathbf{U}_2 + \dots + a^N\mathbf{U}_N \quad \text{avec} \quad a \in [0, a_{max}]$$

- piece-wise continuous representation
- **auto-adaptative** step length \rightarrow Robustness
- no algorithmic parameter



The cornerstone

To compute the Taylor series of the solution-branch :

- Insert the Taylor series

$$u(a) = u_0 + a u_1 + a^2 u_2 + \cdots + a^N u_N$$

- Into the algebraic equation

$$R(u, \lambda) := u + u^2 + \frac{\tan(u)}{1+u} - \lambda = 0$$

- And collect terms with the same powers !

Two techniques :

- use **Automatic Differentiation** to do the job : nice for the user but poor efficiency.
- do a **quadratic recast** of the equations : then the job becomes easy and efficient



Quadratic recast

How to recast the algebraic system $\mathbf{R}(\mathbf{U}) = \mathbf{0}$ in a quadratic way ?

- Goal : find auxiliary variables \mathbf{U}_a and \mathbf{R}_f such that

$$\mathbf{R}_f(\mathbf{U}_f) = \mathbf{C} + \mathbf{L}(\mathbf{U}_f) + \mathbf{Q}(\mathbf{U}_f, \mathbf{U}_f)$$

- with $\mathbf{U}_f = (\mathbf{U}, \mathbf{U}_a)$,
- \mathbf{C} constant,
- \mathbf{L} linear,
- \mathbf{Q} quadratic.

Note that $\mathbf{R}_f(\mathbf{U}_f) = \begin{bmatrix} \mathbf{R}(\mathbf{U}_f) \\ \mathbf{R}_a(\mathbf{U}_f) \end{bmatrix}$ with $\frac{\partial \mathbf{R}_a}{\partial \mathbf{U}_a}$ invertible and $\mathbf{R}(\mathbf{U}_f) = \mathbf{R}(\mathbf{U})$.



The examples of the pendulum

Dimensionless parameters : $m = 1$ and $g = 1$.

Energy of the system :

$$H(\theta) = 1 - \cos(\theta) + \frac{k}{2}\left(\theta - \frac{\pi}{M}\right)^2$$

Equation of the motion :

$$\ddot{\theta} + \sin(\theta) + k\left(\theta - \frac{\pi}{M}\right) = 0$$

Steps :

- $M = 2$ is constant, development about $\theta = 0$:

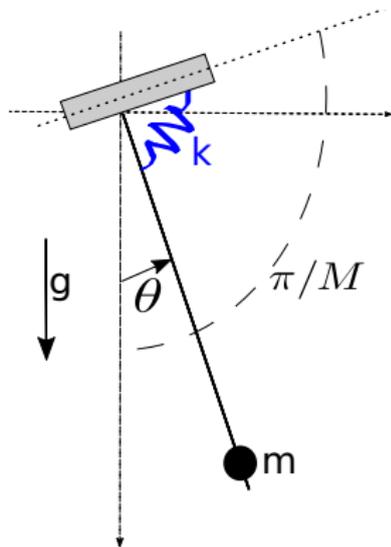
$$\ddot{\theta} + \theta - \frac{\theta^3}{6} + k\left(\theta - \frac{\pi}{2}\right) = 0$$

- $k = 0.1$ is constant, development about $\theta = 0$:

$$\ddot{\theta} + \theta - \frac{\theta^3}{6} + 0.1\left(\theta - \frac{\pi}{M}\right) = 0$$

- Without simplification :

$$\ddot{\theta} + \sin(\theta) + k\left(\theta - \frac{\pi}{M}\right) = 0$$



How to recast polynomials quadratically ?

Let $\mathbf{R}(\mathbf{U}) = \mathbf{R}(u, \lambda) = u^3 + u + 1 - \lambda$.

Let $v = u^2$.

$\mathbf{U} = (u, \lambda)$ and $\mathbf{U}_a = v$ then $\mathbf{U}_f = (\mathbf{U}, \mathbf{U}_a) = (u, \lambda, v)$.

Then \mathbf{R}_f is defined :

$$\mathbf{R}_f(\mathbf{U}_f) = \mathbf{R}_f(u, \lambda, v) = \begin{bmatrix} uv + u + 1 - \lambda \\ v - u^2 \end{bmatrix}$$

And the operators are $\mathbf{C} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$, $\mathbf{L}(\mathbf{U}_f) = \begin{bmatrix} u - \lambda \\ v \end{bmatrix}$, $\mathbf{Q}(\mathbf{U}_f, \mathbf{U}_f) = \begin{bmatrix} uv \\ -u^2 \end{bmatrix}$.



Basic example : Simplified Pendulum

Pendulum subject to an angular spring at position $\theta = \frac{\pi}{2}$, developed around $\theta = 0$.
The equilibrium is given by :

$$r(\theta, k) = \left(\theta - \frac{\theta^3}{6}\right) + k\left(\theta - \frac{\pi}{2}\right)$$

Definition of the auxiliary variables

$$\psi = \theta^2$$

Yields the quadratic recast

$$\mathbf{R}_f(\mathbf{U}_f) = \mathbf{R}_f(\theta, k, \psi) = \begin{bmatrix} \theta - \frac{\theta\psi}{6} + k\theta - k\frac{\pi}{2} \\ \psi - \theta^2 \end{bmatrix}$$

And the operators are $\mathbf{C} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$, $\mathbf{L}(\mathbf{U}_f) = \begin{bmatrix} \theta - k\frac{\pi}{2} \\ \psi \end{bmatrix}$, $\mathbf{Q}(\mathbf{U}_f, \mathbf{U}_f) = \begin{bmatrix} -\frac{\theta\psi}{6} \\ -\theta^2 \end{bmatrix}$.



How to recast fractions quadratically ?

Let $\mathbf{R}(\mathbf{U}) = \mathbf{R}(u, \lambda) = \frac{1}{u} + u - \lambda$.

Let $v = \frac{1}{u}$. v can be defined implicitly through $uv = 1$.

Then \mathbf{R}_f is defined :

$$\mathbf{R}_f(\mathbf{U}_f) = \mathbf{R}_f(u, \lambda, v) = \begin{bmatrix} v + u - \lambda \\ uv - 1 \end{bmatrix}$$

And the operators are $\mathbf{C} = \begin{bmatrix} 0 \\ -1 \end{bmatrix}$, $\mathbf{L}(\mathbf{U}_f) = \begin{bmatrix} u + v - \lambda \\ 0 \end{bmatrix}$, $\mathbf{Q}(\mathbf{U}_f, \mathbf{U}_f) = \begin{bmatrix} 0 \\ uv \end{bmatrix}$.

Here, $\mathbf{R}_a(\mathbf{U}_f) = uv - 1$ and $\frac{\partial \mathbf{R}_a}{\partial \mathbf{U}_a} = \frac{\partial \mathbf{R}_a}{\partial v} = u$. It is invertible if and only if $u \neq 0$.



Simple example : Another Simplified Pendulum

Pendulum subject to an angular spring at position $\theta = \frac{\pi}{M}$, developed around $\theta = 0$.
The equilibrium is given by :

$$r(\theta, M) = \left(\theta - \frac{\theta^3}{6}\right) + 0.1\left(\theta - \frac{\pi}{M}\right)$$

Definition of the auxiliary variables

$$\begin{aligned}\psi &= \theta^2 \\ M_{inv} &= \frac{1}{M}\end{aligned}$$

Yields the quadratic recast

$$\mathbf{R}_f(\mathbf{U}_f) = \mathbf{R}_f(\theta, M, \psi, M_{inv}) = \begin{bmatrix} \theta - \frac{\theta\psi}{6} + 0.1(\theta - M_{inv}\pi) \\ \psi - \theta^2 \\ M_{inv}M - 1 \end{bmatrix}$$



How to recast **everything else** quadratically ?

Let $\mathbf{R}(\mathbf{U}) = \mathbf{R}(u, \lambda) = u - \tan(u) - \lambda$. Let $t = \tan(u)$ and let $z = 1 + t^2$. t and z can be defined by the system :

$$\begin{aligned} dt &= z du \\ z &= 1 + t^2 \end{aligned}$$

These equations are quadratic with respect to the Taylor coefficients of u, t and z . Then \mathbf{R}_f and its differential form $d\mathbf{R}_f$ are defined :

$$\mathbf{R}_f(\mathbf{U}_f) = \mathbf{R}_f(u, \lambda, t, z) = \begin{bmatrix} u - t - \lambda \\ t - \tan(u) \\ z - 1 - t^2 \end{bmatrix} \quad d\mathbf{R}_f(\mathbf{U}_f, d\mathbf{U}_f) = \begin{bmatrix} \text{Not needed} \\ dt - z du \\ \text{Not needed} \end{bmatrix}$$

And the operators are $\mathbf{C} = \begin{bmatrix} 0 \\ 0 \\ -1 \end{bmatrix}$, $\mathbf{L}(\mathbf{U}_f) = \begin{bmatrix} u - t - \lambda \\ 0 \\ z \end{bmatrix}$, $\mathbf{Q}(\mathbf{U}_f, \mathbf{U}_f) = \begin{bmatrix} 0 \\ 0 \\ -t^2 \end{bmatrix}$,

$$d\mathbf{L}(d\mathbf{U}_f) = \begin{bmatrix} 0 \\ dt \\ 0 \end{bmatrix} \quad \text{and} \quad d\mathbf{Q}(\mathbf{U}_f, d\mathbf{U}_f) = \begin{bmatrix} 0 \\ -z du \\ 0 \end{bmatrix}.$$



Transcendental example : Pendulum

Pendulum subject to an angular spring at position $\theta = \frac{\pi}{M}$.
 The equilibrium is given by :

$$r(\theta, k, M) = \sin(\theta) + k\left(\theta - \frac{\pi}{M}\right)$$

Definition of the auxiliary variables, together with the differentiated forms (when needed) :

$$\begin{aligned} s &= \sin(\theta) & ds &= c d\theta \\ c &= \cos(\theta) & dc &= -s d\theta \\ M_{inv} &= \frac{1}{M} \end{aligned}$$

Define $\mathbf{U}_f = (\theta, k, M, s, c, M_{inv})$ yields the "quadratic" recast

$$\mathbf{R}_f(\mathbf{U}_f) = \begin{bmatrix} s + k(\theta - M_{inv}\pi) \\ s - \sin(\theta) \\ c - \cos(\theta) \\ M_{inv}M - 1 \end{bmatrix} \quad d\mathbf{R}_f(\mathbf{U}_f, d\mathbf{U}_f) = \begin{bmatrix} \text{Not needed} \\ ds - cd\theta \\ dc + sd\theta \\ \text{Not needed} \end{bmatrix}$$



End of the Algebraic elements of theory.

Taylor series algebra

- Product of Taylor series $u(a) \times v(a)$:

$$\begin{aligned} & (u_0 + au_1 + a^2u_2 + \dots + a^Nu_N) \times (v_0 + av_1 + a^2v_2 + \dots + a^Nv_N) \\ &= u_0v_0 + a(u_1v_0 + u_0v_1) + a^2(u_2v_0 + u_1v_1 + u_0v_2) + \dots + a^N \sum_{j=0}^N u_{N-j}v_j \end{aligned}$$

It is truncated at order N .

- Differentiation of Taylor series $\frac{\partial u}{\partial a}(a)$:

$$\frac{\partial}{\partial a} (u_0 + au_1 + a^2u_2 + \dots + a^Nu_N) = u_1 + 2au_2 + 3a^2u_3 + \dots + Na^{N-1}u_N$$

The constant coefficient u_0 is not anymore in the development, that goes now up to order $N - 1$.



Manlab 4.0

Let $R(\mathbf{U}) = 0$ be

$$\begin{aligned}r_1(u_1, u_2, \lambda) &= 2u_1 - u_2 + 100 \frac{u_1}{1+u_1+u_1^2} - \lambda &= 0 \\r_2(u_1, u_2, \lambda) &= 2u_2 - u_1 + 100 \frac{u_2}{1+u_2+u_2^2} - (\lambda + \mu) &= 0\end{aligned}$$

Introduce the auxiliary variables :

$$\begin{aligned}v_1 &= 1 + u_1 + u_1 u_1 \\v_2 &= 1 + u_2 + u_2 u_2 \\v_3 &= 1/v_1 \\v_4 &= 1/v_2\end{aligned}$$

- All these expression are quadratic, or easily made quadratic
- **"linear declaration rule"** : an auxiliary variable v_i cannot appear on the left hand side before it has been explicitly defined as $v_i = f(\mathbf{U}, v_1, v_2, \dots, v_{i-1})$. Ensures that $\frac{\partial \mathbf{R}_a}{\partial \mathbf{U}_a}$ is invertible.

Let $\mathbf{U}_a = [v_1, v_2, v_3, v_4]$ be the vector of auxiliary variables
Let $\mathbf{U}_f = [\mathbf{U}, \mathbf{U}_a]$



Manlab 4.0

The original system $R(\mathbf{U}) = 0$ is replaced by the equivalent quadratic one $\mathbf{R}(\mathbf{U}_t)$

$$\begin{aligned}r_1 &:= 2u_1 - u_2 + 100u_1v_3 - \lambda &= 0 \\r_2 &:= 2u_2 - u_1 + 100u_2v_3 - (\lambda + \mu) &= 0 \\r_{aux1} &:= v_1 - 1 + u_1 + u_1 * u_1 &= 0 \\r_{aux2} &:= v_2 - 1 + u_2 + u_2 * u_2 &= 0 \\r_{aux3} &:= v_3 * v_1 - 1 &= 0 \\r_{aux4} &:= v_4 * v_2 - 1 &= 0\end{aligned}$$

Tensor formalism : this quadratic system may be written

$$R_i = C_i + L_{ij}U_j + Q_{ijk}U_jU_k \quad i, j, k = 1, 2, \dots, n$$

with C, L, Q being tensors of order 1, 2 and 3

Here, we have 7 components C_i , 49 components L_{ij} and 343 components Q_{ijk} .

But most of them are zero !



Manlab 4.0 : Sparse tensor formalism

The sparse tensor C , L and Q are defined by the following lists (as in Matlab for a sparse matrix)

- order 1 tensor C

$$iC = [2 \quad 5 \quad 6]$$
$$vC = [-\mu \quad -1 \quad -1]$$

- order 2 tensor L

$$iL = [1 \quad 1 \quad 1 \quad 2 \quad 2 \quad 2 \quad 3 \quad 3 \quad 4 \quad 4 \quad 5 \quad 6]$$
$$jL = [1 \quad 2 \quad 7 \quad 1 \quad 2 \quad 7 \quad 1 \quad 3 \quad 2 \quad 4 \quad 5 \quad 6]$$
$$vL = [2 \quad -1 \quad -1 \quad -1 \quad 2 \quad -1 \quad -1 \quad 1 \quad -1 \quad 1 \quad 1 \quad 1]$$

- order 3 tensor Q

$$iQ = [1 \quad 2 \quad 3 \quad 4 \quad 5 \quad 6]$$
$$jQ = [1 \quad 2 \quad 1 \quad 2 \quad 3 \quad 4]$$
$$kQ = [5 \quad 6 \quad 1 \quad 2 \quad 5 \quad 6]$$
$$vQ = [100 \quad 100 \quad -1 \quad -1 \quad 1 \quad 1]$$

In Manlab 4.0, these lists are **automatically generated** from the quadratic system.



Manlab 4.0 : Sparse tensor formalism

How to get the lists defining the sparse tensor, from the quadratic expression
 $R(X) := 0$?

Polarization formula :

$$C = R(0)$$

$$L(X) = \frac{1}{2} (R(X) - R(-X))$$

$$Q(X, Y) = \frac{1}{4} (R(X + Y) - R(X - Y) - R(Y) + R(-Y))$$



Manlab 4.0 : Sparse tensor formalism

Using these lists, the computation of the residual vector $R(\mathbf{U}) = C + L(\mathbf{U}) + Q(\mathbf{U}, \mathbf{U})$ stand in one (Matlab) line.

```
R =sparse(iC,ones(1,size(iC,2)),vC',neq,1)  
+ sparse(iL,ones(1,size(iL,2)),vL'.*U(jL),neq,1)  
+ sparse(iQ,ones(1,size(iQ,2)),vQ'.*(U(jQ).*U(kQ)),neq,1)
```

For the jacobian matrix $dRdU = L(.) + Q(\mathbf{U},.) + Q(.,\mathbf{U})$

```
dRdU = sparse(iL,jL,sys.vL,neq,ninc)  
+ sparse(iQ,kQ,vQ'.*U(jQ),neq,ninc)  
+ sparse(iQ,jQ,vQ'.*U(kQ),neq,ninc)
```



Manlab 4.0 : Condensation

The linear problem to be solved at each order p reads :

$$\begin{bmatrix} B & A_{aux} \\ A & C \end{bmatrix} \begin{bmatrix} \mathbf{U} \\ \mathbf{U}_{aux} \end{bmatrix} = \begin{bmatrix} F_{aux \ p} \\ F_p \end{bmatrix} \quad \begin{array}{l} \leftarrow R_{aux} \\ \leftarrow R \end{array}$$

Thanks to the "linear declaration rule", the matrix A_{aux} is triangular which allows an easy and cheap block solving

We first solve

$$\left[A - C A_{aux}^{-1} B \right] [U] = \left[F_p - C A_{aux}^{-1} F_{aux \ p} \right]$$

where $\left[A - C A_{aux}^{-1} B \right]$ is the jacobian matrix of the original (non quadratic) system.

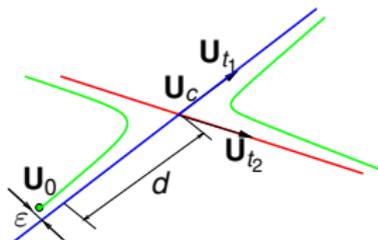


Bifurcation detection using series analysis

Numerical evidence : near a simple bifurcation, a **geometric series** emerge in the Taylor series.

$$\mathbf{U}(a) = \mathbf{U}_0 + a\mathbf{U}_1 + a^2\mathbf{U}_2 + a^3\mathbf{U}_3 + \dots$$

First order analysis : expression of a perturbed branches near a simple bifurcation [Cochelin & Médale, 2013]



$$\mathbf{U}(a) = \mathbf{U}_0 + a\mathbf{U}_{t_1} - \varepsilon \frac{\frac{a}{d}}{(1 - \frac{a}{d})} \mathbf{U}_{t_2}$$

- $\frac{\frac{a}{d}}{1 - \frac{a}{d}} = \frac{a}{d} + (\frac{a}{d})^2 + (\frac{a}{d})^3 + \dots$, a geometric serie with common ratio $\frac{1}{d}$
- After each Taylor series computation, we look for an emerging geometric series. When detected , it is extracted, completed to infinity and replaced by a fraction

$$\mathbf{U}(a) = \underbrace{\mathbf{U}_0 + a\hat{\mathbf{U}}_1 + a^2\hat{\mathbf{U}}_2 + \dots + a^{n-1}\hat{\mathbf{U}}_{n-1}}_{\hat{\mathbf{U}}(a) \text{ cleaned series}} + \frac{a}{d} \left(\frac{1}{1 - \frac{a}{d}} \right) \mathbf{U}_{scale}$$

We get d , \mathbf{U}_{t_2} and can go further the bifurcation thanks to the cleaned series.

